

Optical Description of Mesostuctured Organic-Inorganic Halide Perovskite Solar Cells

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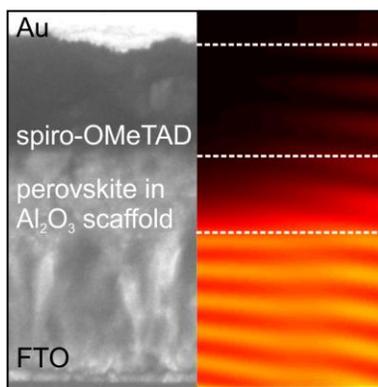
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ABSTRACT Herein we describe both theoretically and experimentally the optical response of solution-processed organic-inorganic halide perovskite solar cells based on mesostructured scaffolds. We develop a rigorous theoretical model using a method based on the propagation of waves in layered media, which allows visualizing the way in which light is spatially distributed across the device and serves to quantify the fraction of light absorbed by each medium comprising the cell. The discrimination between productive and parasitic absorption yields an accurate determination of the internal quantum efficiency. State-of-the-art devices integrating

mesoporous scaffolds infiltrated with perovskite are manufactured and characterized to support the calculations. This combined experimental and theoretical analysis provides a rational understanding of the optical behavior of perovskite cells, and can be beneficial for the judicious design of devices with improved performance. Notably, our model justifies the presence of a solid perovskite capping layer in all the highest efficiency perovskite solar cells based on thinner mesoporous scaffolds.

TOC GRAPHICS



KEYWORDS photovoltaics, perovskite, optical design.

Organic-inorganic halide perovskite solar cells have driven a paradigm shift in photovoltaics (PV) since they are breaking with the sempiternal tradeoff between power conversion efficiency and fabrication cost.¹⁻⁵ Not long after their inception, this solar cell concept is already striding ahead in the emerging PV efficiency race, having reached in the last two years certified efficiency values that significantly surpass all the ones attained for other cells based on solution-processed materials,⁶ and rapidly approaching existing commercial thin-film technologies. This rapid progress has been based on improvements of fabrication methods, charge carrier materials, device architecture, morphology and crystallinity of the perovskite thin films, and the

composition of the perovskite.⁷⁻¹⁹ Another route to boost the efficiency of solar cell devices consists on the optimization of their optical design to maximize light harvesting and charge collection.²⁰ In this regard, efforts have been made to optimize the electro-optical performance of both materials²¹⁻²⁴ and devices.²⁵ In this respect, only cells that make use of flat, evaporated, perovskite layers have been modeled and, to the best of our knowledge, a detailed description of the optical behavior of the complete mesostructured device is still missing, especially understanding the difference between the optical properties of the perovskite when forming a solid crystalline film, in comparison to when infiltrated into a mesoporous scaffold.

Herein, we perform an in-depth experimental and theoretical analysis of the optical effects occurring in state-of-the-art solution-processed organic lead halide perovskite cells. We develop a rigorous theoretical model based on the transfer matrix formalism,²⁶ which allows us to calculate the electric field intensity within the layered structure and thus to visualize the effect of each component of the cell on the spread of the radiation in the device. This permits to estimate the amount of light that is harvested by each absorbing layer in the cell, and consequently to distinguish between productive and parasitic absorption in the PV device. Such discrimination enables the accurate determination of the internal quantum efficiency, which otherwise would be underestimated. To check the suitability of the proposed theoretical model, we compare our results with the experimental reflectance, transmittance and absorptance spectra of actual cells. Our work also provides a theoretical framework in which the optical response of devices integrating photonic enhancing components can be rationalized. We believe such integration may open the door to the realization of perovskite solar cells of improved efficiency due to the maximization of light absorption in extremely thin films.

Figure 1 (a) shows a secondary electron scanning electron microscopy (SEM) image of a cross section of a perovskite solar cell, and Figure 1 (b) a schematic of such PV device. From the bottom side, where the light impinges, the cell is comprised of a fluorine doped tin oxide (FTO) coated glass, covered by a n-type electron collecting TiO_2 compact layer that also acts as a blocking layer. A mesoporous Al_2O_3 layer, which serves as scaffold, is then deposited over the n-type layer followed by the infiltration of the $\text{CH}_3\text{NH}_3\text{PbI}_3$ perovskite material. Please note that solution-processed films typically show a perovskite capping layer, which can be non-uniform in nature, over the scaffold, as we show in Figure 1 (a). The hole transporting material, 2,2',7,7'-tetrakis-(N,N-di-p-methoxyphenylamine) 9,9'-spirobifluorene (spiro-OMeTAD), is then deposited over the perovskite to collect the holes at the gold cathode. We measure the PV performance of the solar cells under investigation. The average device of a batch of 22 cells fabricated in an identical way had a short-circuit photocurrent of $21.7 \pm 1.5 \text{ mA cm}^{-2}$, an open-circuit voltage of $1.02 \pm 0.02 \text{ V}$ and a fill factor of 0.63 ± 0.02 , yielding an efficiency of $13.8 \pm 1.1 \%$ that exhibited a good stabilized power output. The complete PV characterization is provided in the Supporting Information (see Figure S1 and S2).

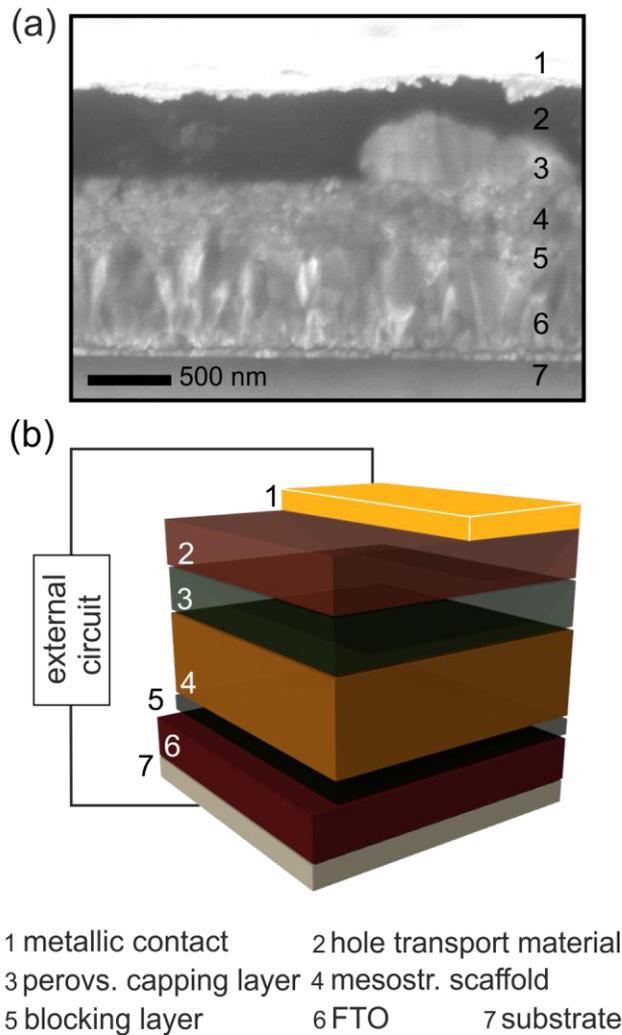


Figure 1. (a) Secondary electron scanning electron microscope image of a cross section of a representative solution-processed perovskite solar cell that integrates a ca. 350 nm-thick mesoporous scaffold. It is comprised of gold as metallic contact, spiro-OMeTAD as hole transport material, a mesostructured Al_2O_3 scaffold infiltrated by $\text{CH}_3\text{NH}_3\text{PbI}_3$, and compact TiO_2 as a blocking layer. The cell is deposited over a fluorinated tin oxide (FTO) coated glass substrate. (b) Schematic of the device.

The perovskite cell is herein modeled through a layered structure, as depicted in Figure 1 (b). The incoming and outgoing media are considered to be air. In our model, the optical effects that arise from the presence of all layers comprising the PV device are accounted for. The optical

constants of the different constituents of the stack, i.e. glass, FTO, spiro-OMeTAD and Au, are taken from literature.²⁷⁻²⁹ The spectral dependence of the perovskite complex refractive index ($N=n+i\cdot k$) is shown in Figure 2 (a). Values of the real (n) and imaginary part (k) are attained by the simultaneous fitting of the Fresnel equations to the reflectance and transmittance measured at normal incidence from thin layers of the perovskite absorber deposited over glass substrates. The attained wavelength-by-wavelength N is employed to calculate a real and an imaginary part that are Kramers-Kronig consistent. Details are provided in the Supporting Information. The optical constants displayed in Figure 2 (a) are in good agreement with those reported for a similar material in References 21, 25 and 30. Similar spectral features are observed both in the real and the imaginary part. However, although the values attained are quantitatively comparable for the extinction coefficient, a clear difference in the mean value of the real part, ranging between 2 and 2.5, is observed between the different reported data (see Figure S4 in the Supporting Information). We attribute this discrepancy to the different experimental routes, from wet chemistry to vapor deposition, followed to prepare the perovskite absorber.

We employ an effective medium approximation to account for: i) the rough FTO surface coated by the thin compact layer, ii) the perovskite infiltrated mesostructured scaffold, and iii) the non-uniform nature of the interface between the perovskite overlayer and the spiro-OMeTAD layer. In order to determine the effective optical constants of such media, we considered different equations, i.e. volume-weighted average, Cuming and Maxwell-Garnett. Regarding i) and iii), in view of the cross sections observed in the SEM, considering an equal contribution to the refractive index of the transition middle layer from the materials at both sides of the interface seems reasonable. In the case of the mesostructured Al_2O_3 scaffold, a 46% porosity prior to perovskite infiltration was attained from the fitting of its experimental reflectance, assuming that

the thickness and the permittivity of the alumina are known from the analysis of SEM images and the scientific literature,³¹ respectively. The very similar results attained from the different effective medium equations employed led us to consider the simplest approximation, i.e. the volume-weighted average, to calculate the effective optical constants.

Our theoretical model serves to describe the optical response, i.e. reflectance (R), transmittance (T) and absorptance (A), of a representative cell shown as, respectively, orange, red, and black solid lines in Figure 2 (b). Measurements performed in an integrating sphere show that the A of the device reaches values above 90% at 500 nm, where the extinction coefficient is maximum, shows values above 80% from 400 to 700 nm, and significantly diminishes at ca. 800 nm, at the edge of the perovskite absorber electronic band gap. As in the experiments, the calculation considers an incident wave vector that impinges perpendicularly to the electrode and therefore to the stacking of dielectric layers, although the description of angular and polarization effects would also be possible if necessary. To obtain the R and T of the cell, the intensity of the electric field in the incident and outgoing medium, respectively, are calculated by solving the set of equations established by imposing the continuity of the electric and magnetic fields across each interface using a method based on the transfer matrix formalism (see Reference 32 for details). Notice that the thick glass substrate can be considered in the model as a layer that does not give rise to interference effects since the coherence length of the incident light is much shorter than its thickness.³³ As a result the calculated spectra in Figure 2 (b) do not show the very short period fringes, which would arise from the presence of an ideal flat ca. 1 mm-thick layer. The total absorptance is estimated as the fraction of light that was neither reflected nor transmitted as $1-R-T$. A linear least-squares method is employed to fit the experimental R and T. We consider the thickness of the different layers comprising the multilayer stack as fitting parameters. The values

extracted from the SEM are taken as initial values. Fair agreement between theory (dashed lines) and experiment (solid lines) is found as displayed in Figure 2 (b). It can be clearly seen the correspondence between spectral features in R and A. As the wavelength increases, the extinction coefficient of the perovskite diminishes and both R and T increase. Note that our model does not account for the effect of diffuse scattering. In fact, the diffuse reflectance may well explain the small discrepancy observed between measured and calculated R and, consequently, between measured and calculated A in the spectral range comprised between ca. 700 and 800 nm, where the fraction of light diffusely reflected shows values between ca. 2 % and 10 %. This results in an overestimation of the fraction of light absorbed by the device at longer wavelengths. Note that the air mass coefficient in this range greatly reduces, and therefore the impact of the inaccuracy of our model in the overall response of the solar cell is not significant. The spectral dependence of the experimental total and diffuse reflectance is shown in Fig. S5 of the Supporting Information.

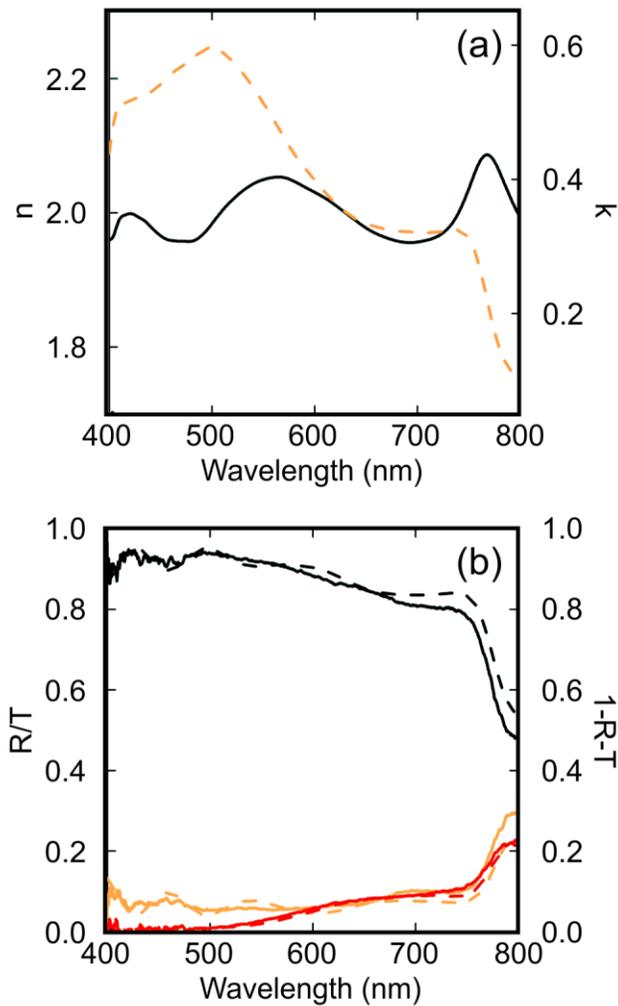


Figure 2. (a) Spectral dependence of the real (black solid line) and imaginary part (orange dashed line) of the refractive index of the $\text{CH}_3\text{NH}_3\text{PbI}_3$ perovskite absorber. Values were obtained from fits of the Fresnel equations to reflectance (R) and transmittance (T) spectra measured at normal incidence from thin layers of perovskite. (b) R (orange lines), T (red lines) and total absorptance ($1-R-T$) spectra (black lines) calculated (dashed lines) and measured (solid lines) from a representative device comprising a 350 nm-thick mesoporous Al_2O_3 scaffold infiltrated by perovskite.

We have also calculated the spatial distribution of the square magnitude of the electric field in the multilayer stack. Figure 3 (a) shows the calculated spatial (vertical axis) and spectral

(horizontal axis) distribution of the electric field intensity enhancement (I/I_0), i.e. near-field intensity normalized by the incident intensity, along a cross section of the PV device. Light impinges from the bottom. The glass-FTO interface is sited at 0 μm in the vertical axis. The interference of all beams reflected and transmitted at each interface determines the way in which the radiation distributes over the solar cell for each wavelength. Different wavelengths propagate distinctly through the device. We can observe that the intensity at ca. 500 nm decreases very rapidly in the absorbing scaffold until it vanishes within the perovskite overlayer. In contrast, at 750 nm, where the extinction coefficient of the perovskite absorber is reduced, the penetration of the optical field in the device is significantly larger. The incoming light reaches the last layers of the solar cell, which yields a non-zero transmittance -see Figure 2 (b)-. The calculation of the spatial distribution of the electric field intensity inside the solar cell allows computing the fraction of light absorbed by each constituent of the PV device (A_j) according to

$$A_j = 2\pi \int_{x_j} \frac{I(x_j, \lambda)}{I_0(\lambda)} \frac{2n_j k_j}{\lambda} dx_j$$

where the subscript j refers to each layer comprising the cell, and λ is the wavelength of the radiation. The integral extends over the volume occupied by each medium, which can be reduced to one dimension (x_j) due to the symmetry of the system. Figure 3 (b) displays the fraction of light absorbed by the different absorbing materials that constitute the cell, i.e. FTO (red dotted line), spiro-OMeTAD (brown short dashed line), perovskite (black solid line), and Au (orange dashed line). Thus, our model permits to quantify the optical losses in a perovskite solar cell, and discriminate between productive, i.e. the fraction of light absorbed by the perovskite that generates photocurrent, and parasitic or non-productive absorption in the other component layers. The solar spectrum weighted integrated absorptance (SSWIA), defined as the fraction of

light absorbed by the perovskite weighted across the solar spectrum, between 400 to 800 nm, is 82.9% for the cell under investigation. Note that the total fraction of unproductive light absorbed is below 6% throughout the spectrum, being ca. 2% at 500 nm. In contrast, the specular reflectance is above 5% across the spectrum, reaching values as high as ca. 15% at 750 nm.

The external quantum efficiency (EQE) measured from a representative perovskite PV device is displayed as a black solid line in Figure 3 (c). EQE is defined as the ratio of collected carriers to the incident photons. The internal quantum efficiency (IQE) of a solar cell is typically calculated from the ratio of its EQE and A .¹⁰ The presence of parasitic absorption in the device leads to underestimate the IQE of the solar cell. Using our optical model, it is possible to calculate only the fraction of light absorbed within the perovskite absorber -see Figure 3 (b)-, which enables an accurate determination of the IQE. The IQE, shown as an orange dashed line in Figure 3 (c), is relatively stable over ca. 80% from 450 to 750 nm, indicating that, despite the fact that each wavelength is preferentially absorbed in a different region of the perovskite layer, as revealed by profiles like the one shown in Figure 3(a), photogenerated carriers are collected with equal efficiency in the contacts. Our optical analysis shows that it should be possible to further improve the efficiency of perovskite solar cells by optimizing harvesting of solar radiation in the far red region of the electromagnetic spectrum. This can be achieved by integrating optical elements that selectively enhance the productive absorption of the cell at those wavelengths, or by coating the outer glass with broadband antireflection coatings to minimize reflection losses.

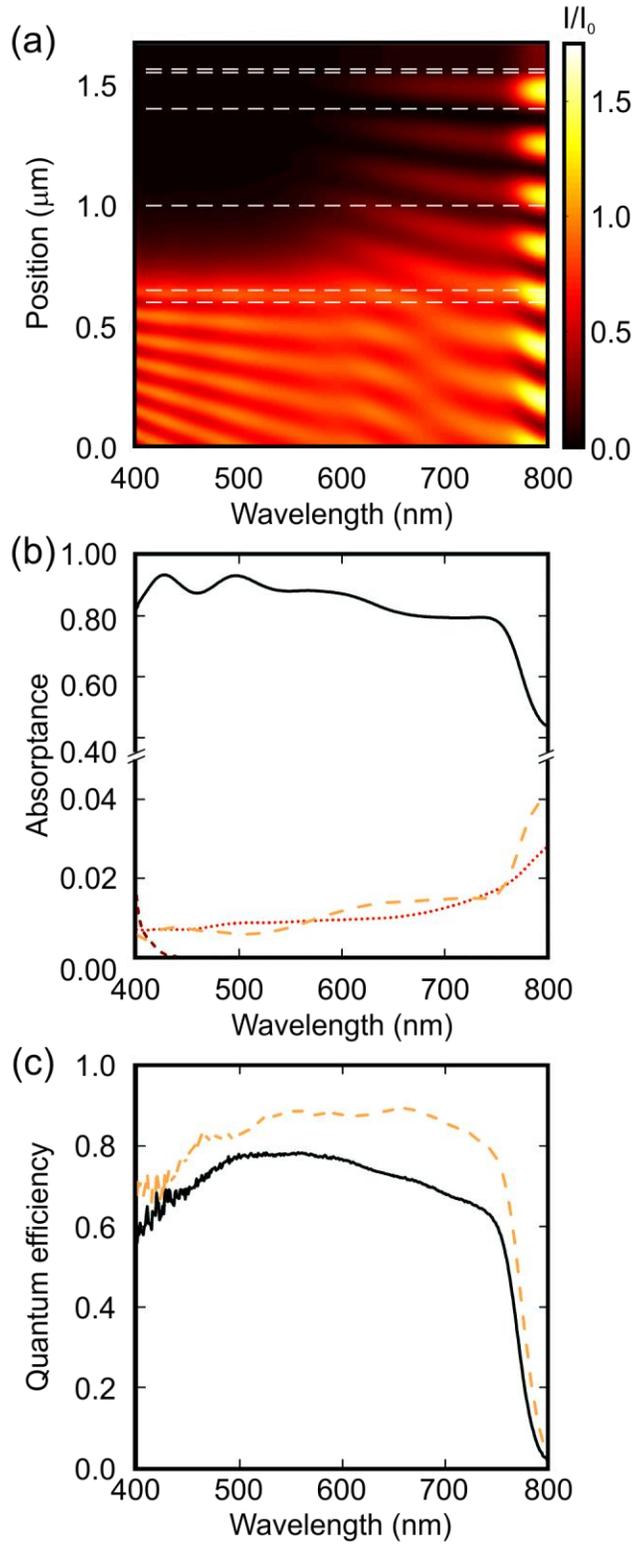


Figure 3. (a) Calculated spatial (vertical axis) and spectral (horizontal axis) distribution of the electric field intensity enhancement (I/I_0), i.e. near-field intensity normalized by the incident

intensity, along a cross section of the perovskite solar cell. Calculations were carried out considering the multilayer parameters extracted from the fittings to reflectance and transmittance measurements. Horizontal dashed lines are guides to the eye to delimit the interfaces between media in the device. From top to bottom: air, Au, spiro-OMeTAD, perovskite overlayer, perovskite-infiltrated Al_2O_3 scaffold, TiO_2 compact layer and FTO. (b) Spectral dependence of the fraction of light absorbed by the different absorbing materials comprising the device: FTO (red dotted line), spiro-OMeTAD (brown short dashed line), perovskite (black solid line), and Au (orange dashed line). (c) Experimental external quantum efficiency (black solid line) and internal quantum efficiency (orange dashed line) estimated from the calculation of the fraction of light absorbed by the perovskite material.

Finally, in Figure 4 (a), we make use of our theoretical model to extrapolate the SSWIA of devices featuring infiltrated mesostructured Al_2O_3 scaffolds as a function of the thickness of the hole transport layer (HTL). Please note that the SSWIA defined hereby would be directly proportional to the estimated short circuit photocurrent if a charge collection efficiency of 100% is assumed. It can be observed that the SSWIA is larger for thicker scaffolds, due to a larger amount of absorbing material. More interestingly, the SSWIA shows an oscillatory behavior with the spiro-OMeTAD layer thickness for a fixed scaffold. Similar oscillatory profiles are attained for scaffolds of different thickness, as shown in Figure 4 (a). As an example, we observe that for a 300 nm-thick perovskite infiltrated scaffold, the SSWIA is 72% for cells comprising a HTL with thickness of 100 or 320 nm, whereas it reaches 75% for a 220 nm-thick HTL. Figure 4 (b) shows the spectral dependence of the fraction of light absorbed by the perovskite material ($A_{\text{perovskite}}$) when infiltrated in mesostructured scaffolds of the same thickness but different composition, namely Al_2O_3 , SiO_2 and TiO_2 . The differences observed may be attributed to the difference in the refractive index of the scaffolds, being TiO_2 the highest and SiO_2 the lowest among the ones considered. One may note that the higher the refractive index, the higher the reflectance, and therefore, the lower the absorptance. Such variations can be further quantified

through the SSWIA parameter, attaining values of 72, 75 and 76%, for the perovskite infiltrated TiO_2 , Al_2O_3 and SiO_2 scaffolds, respectively. In Figure 4 (b), we also plot the $A_{\text{perovskite}}$ for a solar cell that integrates a solid perovskite film of the same thickness (300 nm). The presence of a larger amount of perovskite absorber within the photoactive region leads to almost full absorption, reaching a SSWIA value as high as 88%. Our model also serves to calculate the thickness of the scaffold that would provide a similar SSWIA, attaining thickness values of 600, 570 and 540 nm for mesostructured scaffolds made of TiO_2 , Al_2O_3 and SiO_2 , respectively. Thus, our analysis presents the possibility of finding the material features needed to attain scaffold based perovskite PV devices in which light harvesting is as efficient as in flat bulk perovskite layers. It can also be helpful for optimizing vapor-deposited cells in which extremely uniform films with an accurate thickness control can be achieved.¹¹

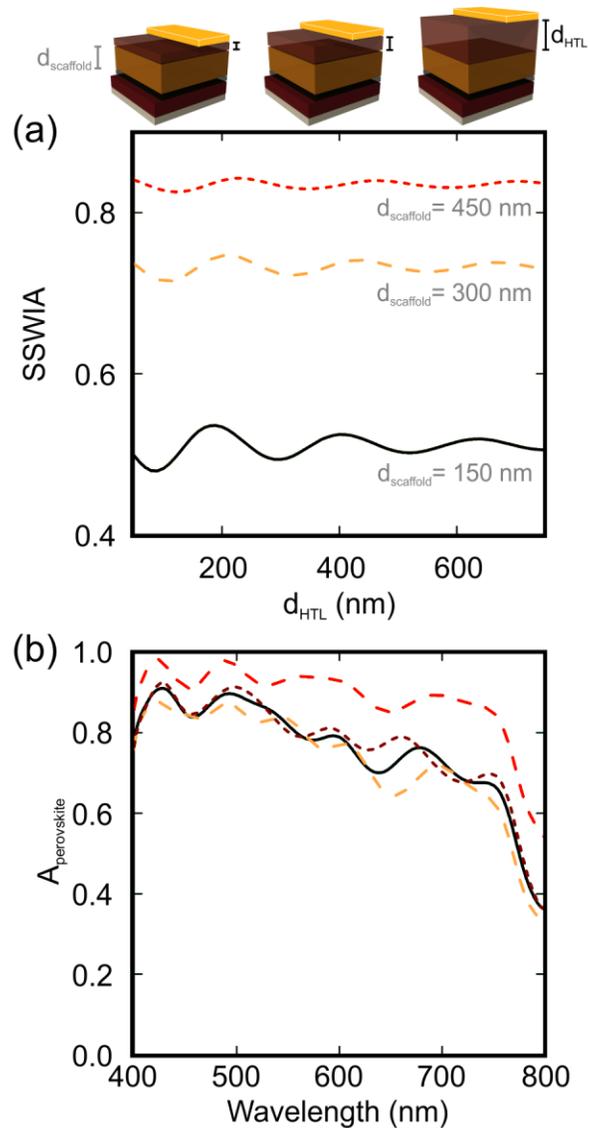


Figure 4. (a) Calculated solar spectrum weighted integrated absorptance (SSWIA) as a function of the hole transport layer (HTL) thickness for photovoltaic devices comprising perovskite-infiltrated mesoporous Al_2O_3 scaffolds with a thickness of 150 nm (black solid line), 300 nm (orange dashed line), and 450 nm (red short dashed line). (b) Spectral dependence of the productive absorptance ($A_{\text{perovskite}}$) of solar cells, in which the perovskite infiltrates a 300 nm-thick mesostructured scaffold made of: SiO_2 (brown short-dashed line), Al_2O_3 (black solid line) and TiO_2 (orange dashed line). For comparison we present as red dashed line the $A_{\text{perovskite}}$ of a solar cell that integrates a solid perovskite film of the same thickness, i.e. 300 nm. We note that

the perovskite absorber only occupies 50% of the volume within the photoactive region and that there is no capping layer considered in the calculations.

In summary, we have developed a rigorous theoretical model that describes the optical behavior of organic-inorganic halide perovskite solar cells. Our theoretical results were confirmed with experimental measurements from state-of-the-art solution-processed devices, although the proposed model could be also employed to describe the optical response of other layered perovskite based PV devices, for instance planar heterojunction solar cells prepared by evaporation solution processing. It serves to visualize the spatial distribution of the radiation within the cell, which allows quantifying the fraction of light absorbed by each constituent of the device, being possible to discern the radiation that actually contributes to generate photocurrent. This allows us to perform an accurate estimation of the internal quantum efficiency of the solar cell. Finally, we have extrapolated our model to describe the influence, due to optical interference, of the features of the different constituents of the cell, such as the thickness of the hole transporting layer, on the light harvesting of solar radiation by the PV device. Insight is also provided on the effect of scaffolds of different composition on the total amount of light harvested by the perovskite absorber, as well as on the thickness required for each type of scaffold to reach the same light absorption than a flat dense perovskite layer. Our results hence open a new avenue for the optical design of perovskite solar cells with improved efficiency.

Experimental methods.

Synthesis of perovskite. Methylamine iodide ($\text{CH}_3\text{NH}_3\text{I}$) was prepared by reacting methylamine, 33 wt% in ethanol (Sigma-Aldrich), with hydroiodic acid (HI) 57 wt% in water (Sigma-Aldrich), at room temperature. Typical quantities employed are 24 mL of methylamine, 10 mL of hydroiodic acid and 100 mL of ethanol. Upon drying at 100°C , a white powder was formed,

which was placed overnight in a vacuum oven and rinsed with ethanol before use.⁹ To obtain the perovskite solution, both the $\text{CH}_3\text{NH}_3\text{I}$ and the PbCl_2 (Sigma-Aldrich) were dissolved in anhydrous N,N-Dimethylformamide (DMF) at a 3:1 molar ratio with final concentrations of ca. 40 wt%.

A modification of this method, in which $\text{Pb}(\text{CH}_3\text{COO})_2$ is used as perovskite precursor instead of PbCl_2 , was employed to fabricate smooth perovskite flat layers with improved film morphology while keeping the chemical composition unchanged.

Device fabrication. All details regarding the fabrication of the solar cells can be found elsewhere.³⁴ In short, FTO patterned glass (Pilkington TEC 7, 7 Ω/sq) was cleaned sequentially in Hellmanex, milliQ water, acetone, ethanol and oxygen plasma. A TiO_2 compact layer was deposited by spin coating a 253 mM titanium isopropoxide precursor (diluted in a mildly acidic anhydrous ethanol solution) at a speed of 2000 rpm for 60 s followed by sintering at 500°C during 45 minutes. After cooling to room temperature an Al_2O_3 scaffold was spin coated at 2500 rpm for 45s from a colloidal dispersion of <50nm Al_2O_3 nanoparticles (Sigma-Aldrich, product number 702129), followed by drying at 150°C for 30min. Throughout all experiments the scaffold thickness was kept constant at ca. 350 nm by diluting the Al_2O_3 nanoparticles dispersion with ethanol in a 1:2 volume ratio. To fabricate the solar cells, Al_2O_3 scaffolds were infiltrated using a 40 wt% perovskite solution by spin-coating at 2000 rpm for 45 s in a nitrogen-filled glovebox. After the spin-coating process, samples were annealed at 100°C for 2h. The spiro-OMeTAD hole-transporting layer was then deposited from a 80 mM chlorobenzene solution containing additives of lithium bis(trifluoromethanesulfonyl)imide and 4-tert-butylpyridine. Finally, gold electrodes were thermally evaporated under vacuum of ca. 10^{-6} Torr, at a rate of ca. 0.1 nm/s, to complete the devices.

Structural characterization. Cross-section field emission scanning electron microscopy images of PV devices were taken by using a microscope Hitachi 5200 operating at 5kV.

Optical characterization. The spectral dependence of the reflectance and transmittance of the solar cells was obtained using an integrating sphere (Labsphere RTC-060-SF), a halogen lamp (Ocean Optics HL-2000) as light source, and a spectrometer (Ocean Optics USB 2000) as detector.

Photovoltaic characterization. The current density–voltage curves were measured (2400 Series SourceMeter, Keithley Instruments) under simulated AM 1.5 sunlight at 100 mWcm^{-2} irradiance generated by an Abet Class AAB sun 2000 simulator, with the intensity calibrated with an NREL calibrated KG5 filtered Si reference cell. The mismatch factor was calculated to be less than 1%. The solar cells were masked with a metal aperture to define the active area, typically 0.0625 cm^2 (measured individually for each mask) and measured in a light-tight sample holder to minimize any edge effects and ensure that the reference and test cells are located in the same spot under the solar simulator during measurement. EQE was measured via Fourier-transform photocurrent spectroscopy using a Bruker Vertex 80v Fourier Transform Interferometer with tungsten-halogen lamp source, CaF_2 beam splitter, a Stanford Research SR570 current preamplifier and custom built control electronics. A forward bias of 1.4 V was applied to devices for a period of 20s before photocurrent spectra were recorded. EQE spectra were calibrated to a Newport-calibrated reference Si solar cell with a known EQE. The solar cells were masked with a metal aperture to define an active area of 0.0625 cm^2 .

ASSOCIATED CONTENT

Supporting Information. Additional photovoltaic and optical characterization is included as supplemental material. This material is available free of charge via the Internet at <http://pubs.acs.org>.

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Notes

During the review process of this manuscript two related articles discussing the optical modeling of planar perovskite solar cells were published (References 35 and 36).

The authors declare no competing financial interests.

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